











Practice-Relevant Teachingof Gas Turbine Performance

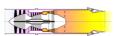
GPPS-TC-2025-0109 Presentation by Joachim Kurzke





















Commercial Airliner 1958 JT3C Turbojet



Should teaching gas turbine performance begin with the turbojet?



That's what I said during the presentation

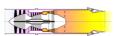


Fig. 100



















Commercial Airliner 2023 CFM Leap Turbofan





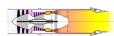
Could teaching also begin with the turbofan?













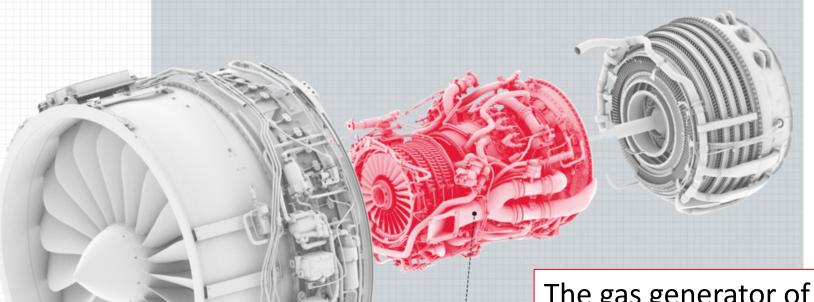








CFM56-3 Modular Design



The heart of any aircraft gas turbine configuration is a gas generator!

The gas generator of the turbofan should be the starting point, and it is from there that we can begin to understand the rest of the system!

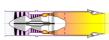


Gas

Generator

has









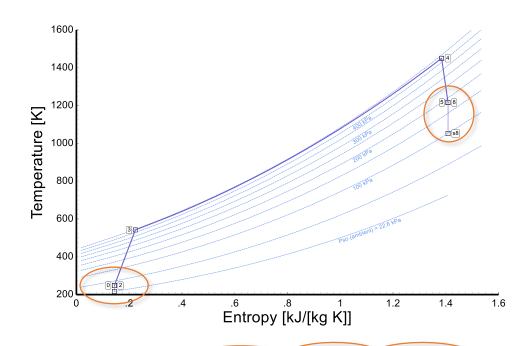






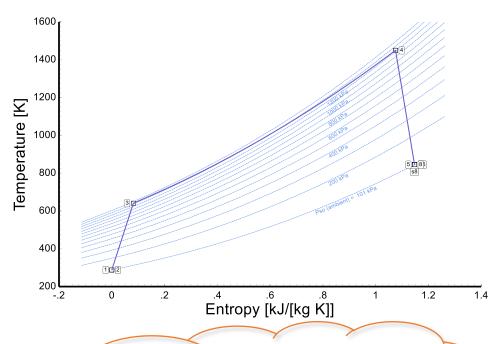
Introduction to the Thermodynamics of Gas Turbines

Turbojet @ 36000ft/0.85



In fact, the operating cycle of a turbojet at 36,000 feet and Mach 0.85 is more complex than that of a gas generator!

Turboshaft SLS



The simplest way to introduce students to the field of gas turbine performance is to model the cycle of the gas generator as a turboshaft on a sea-level test bed!











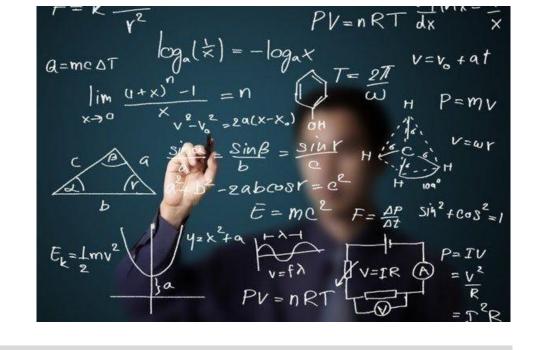






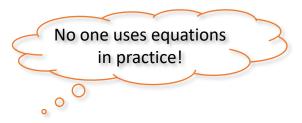






About Equations

... are they suited for realistic gas turbine performance calculations?

























Thermal Efficiency

The Academic Definition

$$\eta_{th} = \frac{\Delta H_T - \Delta H_C}{\Delta H_B}$$

ΔH = specific work in kW per kg/s mass flow

$$\eta_{th} = \frac{\frac{\gamma_T}{\gamma_T - 1} * R_T * \frac{T_4}{T_2} * \left[1 - \left(\frac{P_2}{P_3} \right)^{\frac{\gamma_T - 1}{\gamma_T}} \right] * \eta_T - \frac{\gamma_C}{\gamma_C - 1} * R_C * \left[\left(\frac{P_3}{P_2} \right)^{\frac{\gamma_C - 1}{\gamma_C}} - 1 \right] / \eta_C}{\left(\frac{T_4}{T_2} - \frac{T_3}{T_2} \right) * \left(\frac{\gamma_C}{\gamma_C - 1} * R_C + \frac{\gamma_T}{\gamma_T - 1} * R_T \right) / 2}$$

This equation uses different isentropic exponents γ_{C_i} , γ_{T} and gas constants R_{C_i} , R_{T_i} for the compressor and turbine. Efficiencies η_{C_i} , η_{T_i} are isentropic.

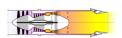






















Thermal Efficiency – Academic Definition

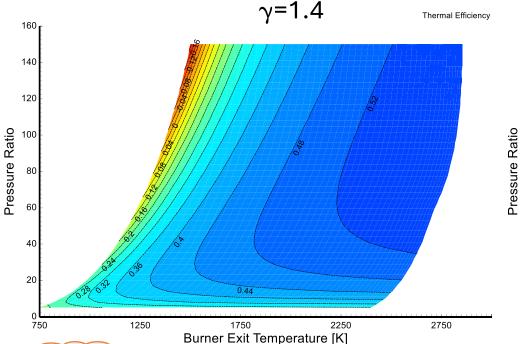
Effect of Isentropic Exponent

160

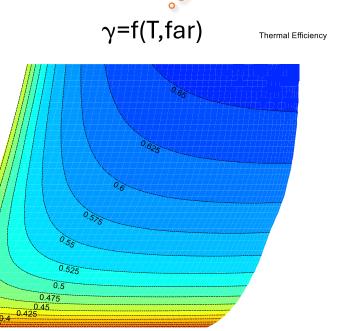
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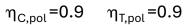
120

With constant isentropic exponent:
The higher the burner exit
temperature, the greater the
thermal efficiency.



With true gas properties:
The higher the pressure ratio,
the greater the thermal
efficiency.





0.275 0.30.325



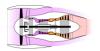
Burner Exit Temperature [K]

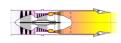


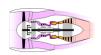
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F. It

Jim.

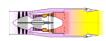






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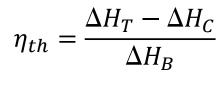




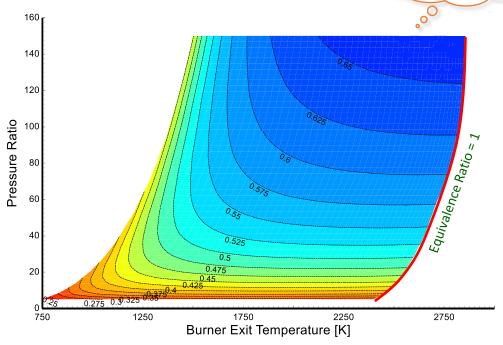


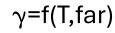
Two Definitions of Thermal Efficiency

Academic





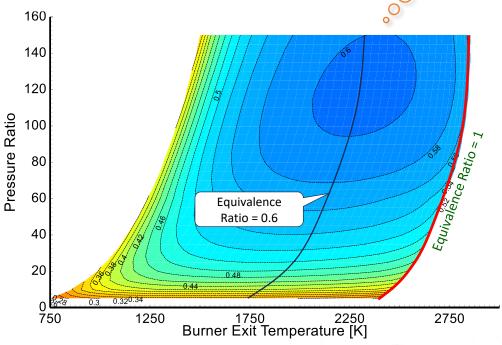




Practice

$$\eta_{th} = \frac{\Delta H_T - \Delta H_C}{W_F \times FHV}$$

There is an optimum along the line where the equivalence ratio is equal to 0.6.



$$\eta_{T,pol}$$
=0.9

$$Equivalence\ ratio = \frac{far}{far_{stoiciometri}}$$





















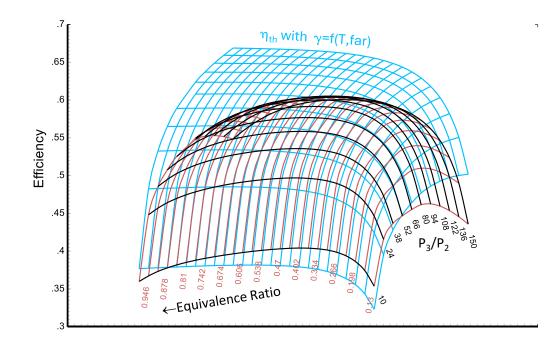
Thermal Efficiency – The Numbers

Academic

$$\eta_{th} = \frac{\Delta H_T - \Delta H_C}{\Delta H_B}$$

Practice

$$\eta_{th} = \frac{\Delta H_T - \Delta H_C}{W_F \times FHV}$$



The academic definition of thermal efficiency yields numbers that are not relevant in practice.























Observations

- The result for constant γ is misleading because it says that the highest burner exit temperature gives the highest thermal efficiency.
- The result for γ =f(T,far) is misleading also because it says that the highest pressure ratio gives the highest thermal efficiency.
- The pressure ratios of up to 150 considered have nothing in common with those of real gas turbines.
- The heat addition method is not included in the academic definition of thermal efficiency.
 - In practice, heat is added by burning fuel.
 - The achievable temperature is limited by stoichiometric combustion
 - The slope $\Delta T/\Delta W_f$ decreases with increasing fuel-air-ratio until $\Delta T/\Delta W_f$ =0 for stoichiometric combustion















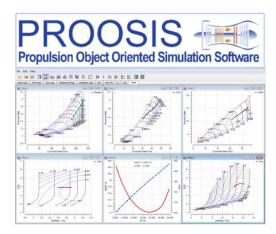












Performance Software

The tool used in practice

GasTurb 8 Professional

1998





















Pressure Ratio

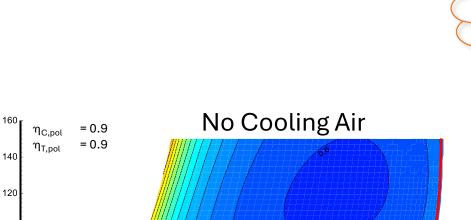
1250





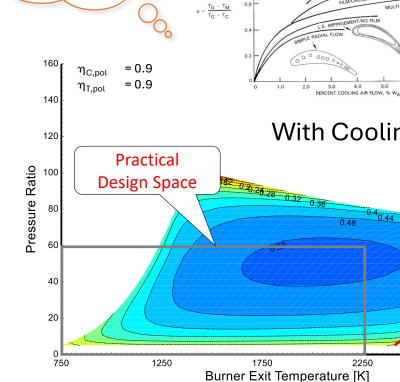


A More Realistic Efficiency Calculation

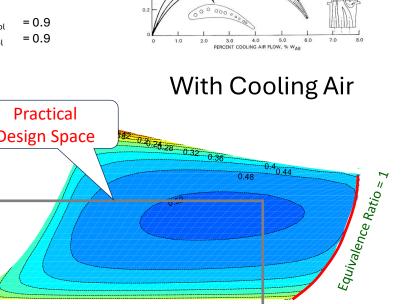


1750

Burner Exit Temperature [K]



The amount of cooling air needed depends on both the gas temperature and the



2750

2750

Fi Im Imm











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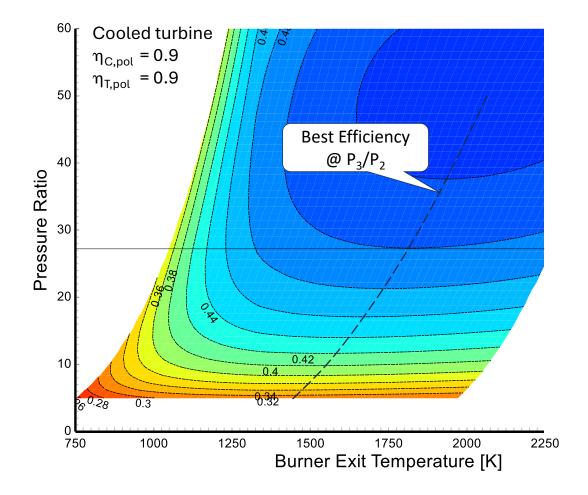


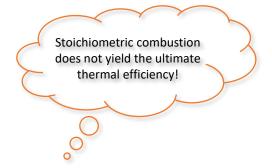






Practical Design Space Thermal Efficiency





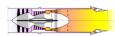














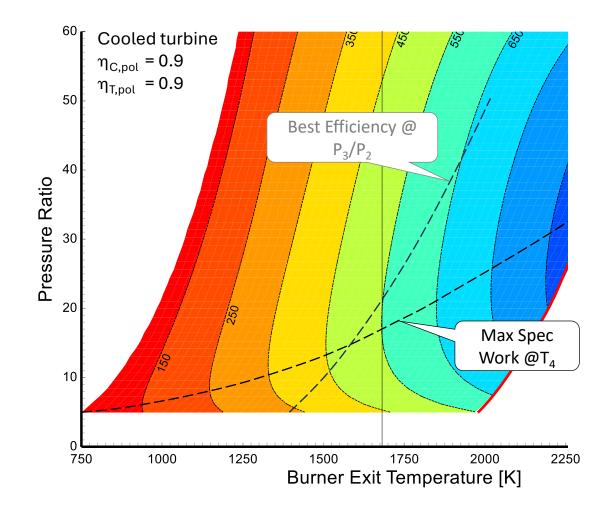








Practical Design Space Specific Power



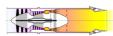
Specific power increases with burner exit temperature















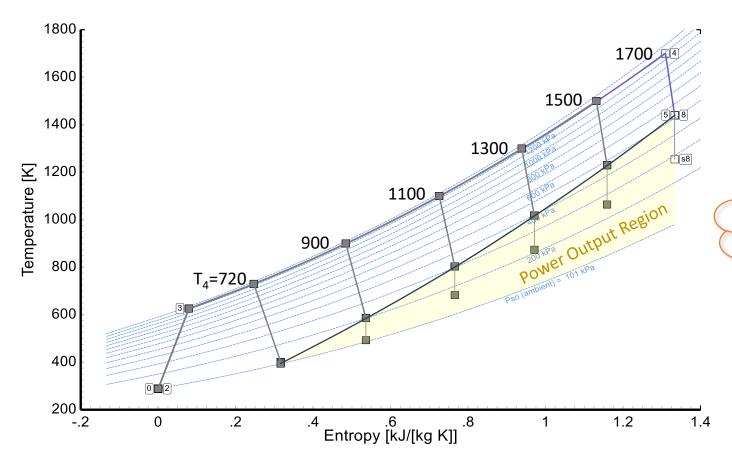






Why Increases Specific Power with T₄?

Pressure Ratio = 12



Because the isobar lines diverge. No equation is needed to explain why specific work increases with burner exit temperature!

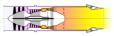






















De-Mystify Your Performance Software

... by doing calculations manually

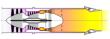












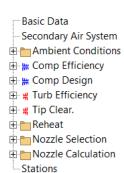












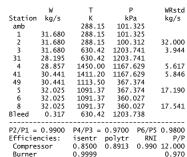








Out



0.8900 0.8757 1.798 3.178

Spool mech Eff 0.9999 Nom Spd 12499 rpm

FN TSFC	=		
FN/W2	=	832.50	m/s
Prop Eff	=	0.0000	
eta core	=	0.3884	
WF	=	0.66194	kg/s
s NOx	=	0.28659	
XM8	=	1.0000	
A8	=	0.0773	m²
P8/Pamb	=	3.5532	
WB1d/W2	=	0.01000	
Ang8	=	20.00	deg
CD8	=	0.9600	_
WC1N/W2	=	0.05000	
WC1R/W2	=	0.05000	
Loading	=	100.00	%
e45 th	=	0.87139	
far8	=	0.02111	
PWX	=	0.00	kW
	TSFC FN/W2 Prop Eff eta core WF s NOx XM8 A8 P8/Pamb WB1d/W2 Ang8 CD8 WC1N/W2 WC1R/W2 Loading e45 th far8	TSFC = FN/W2 = Prop Eff = eta core = WF = \$ \$NO\$ = \$XM\$ = A8 Ps/Pamb = WB1d/W2 = AN0\$ = UC1N/W2 = WC1N/W2 = Uoading = e4\$ th = far8 = \$ \$100 =	TSFC = 25.085 FN/W2 = 832.50 Prop Eff = 0.0000 eta core = 0.3884 WF = 0.66194 S NOX = 0.28659 XM8 = 1.0000 A8 = 0.0773 PS/Pamb = 0.773 Ang8 = 20.000 CD8 = 0.0900 WC1N/W2 = 0.05000 WC1N/W2 = 0.05000 WC1R/W2 = 0.05000 UC1R/M2 = 0.050000 UC1R/M2 = 0.05000 UC1R/M2 = 0.050000 UC1R/M2 = 0.050000 UC1R/M2 = 0.050000 UC1R/M2 = 0.050000 UC1R/

Net Thrust
Thrust Specific Fuel Consumption
Specific Thrust

Propulsion Efficiency
Core Efficiency

Fuel Flow
NOX Severity Parameter
NOZZle Throat Mach No.
Geometric NozZle Throat Area
NOZZle Throst Mach Specific NozZle Pressure Ratio
Bleed Air Flow/Mass Flow W2
NozZle Petal Angle
NozZle Petal Angle
NozZle Discharge Coefficient
Turbine NozZle Guide Vane Cooling Air / W2
Turbine Rotor Cooling Air / W2

Nozzle Discharge Coefficient Turbine Nozzle Guide Vane Cooling Air / W2 Turbine Rotor Cooling Air/ W2 Burner Loading in % of the Cycle Design Point Value Thermodynamic Turbine Efficiency Nozzle Throat Fuel-Air-Ratio Power Offtake



Turbine



















About Performance Software

 Gas turbine performance calculation programs differ from those of computational fluid dynamics (CFD) and finite element analysis (FEA) in one important aspect:

Their output can be easily reproduced on a pocket computer or with Excel.

• Doing that is not just an academic exercise, but often necessary in practical engineering when partners in a collaborative project arrive at different results.





Calculation of the Cycle by Hand











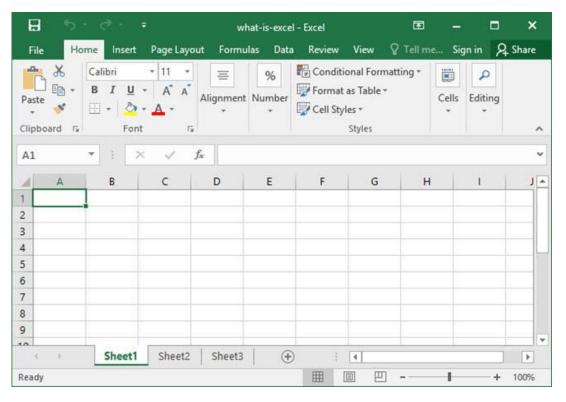


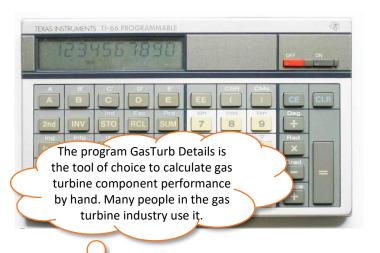


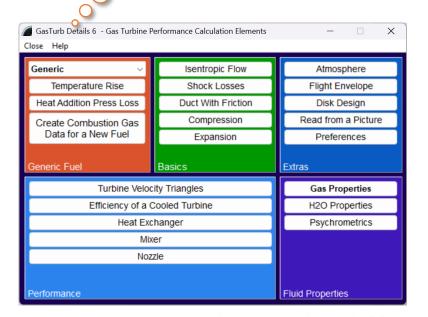












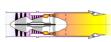




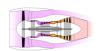












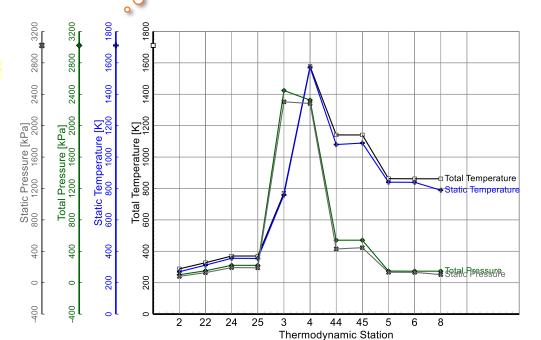


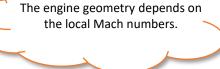


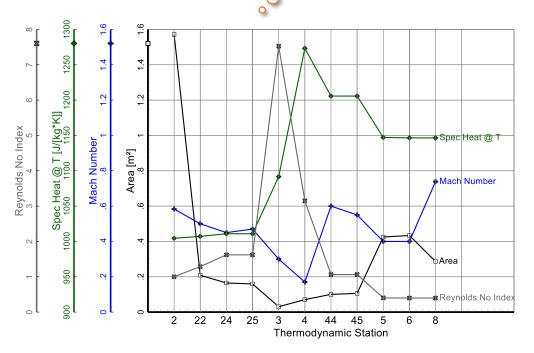


Cycle DataCFM56-3 Take Off

The cycle calculsation yields the total pressures and temperatures.







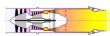














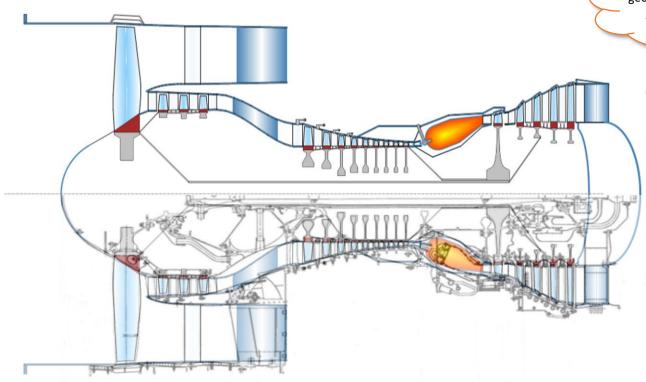








Geometry Model of the CFM56-3 Turbofan



Students will find it challenging and interesting to reproduce the geometry of an engine based on a given cross-cut and publicly available cycle data.























Visualizing the Results

... a picture is worth a thousand words















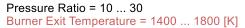


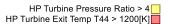


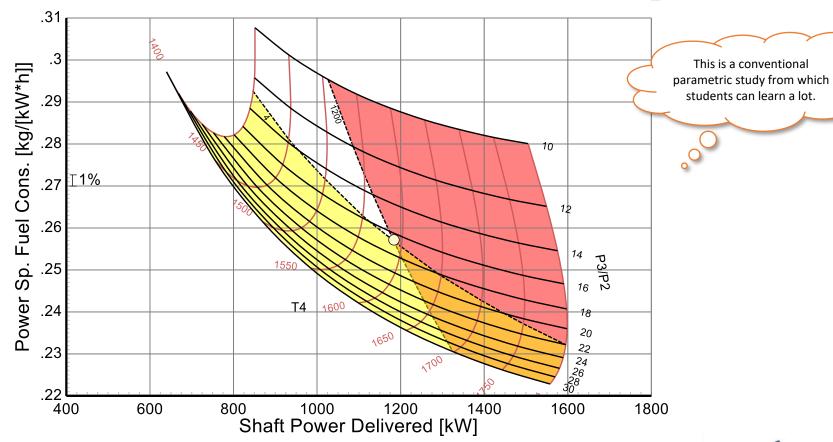




Parametric Study Design Space









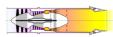
This is a conventional

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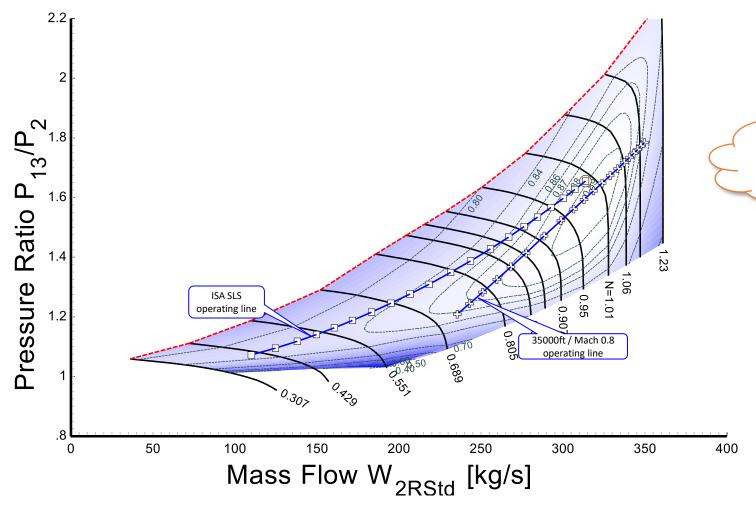








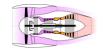
Operating Lines in the Fan Map

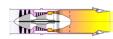


Using colors makes graphics easier to understand and remember.







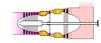




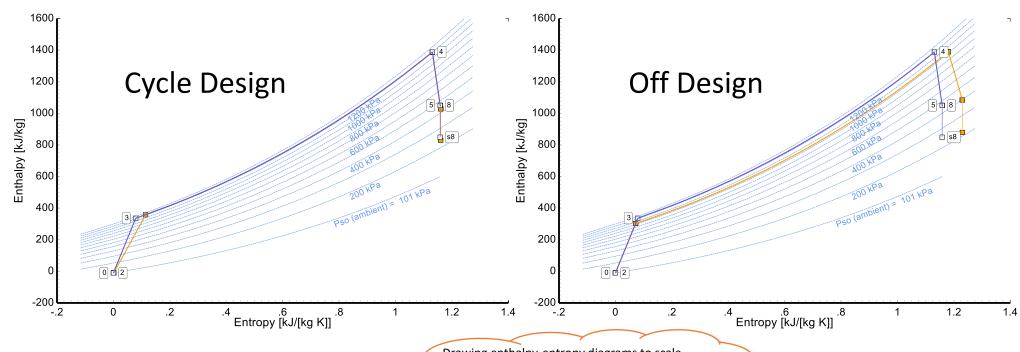








Enthalpy-Entropy Diagram Effect of -5% Compressor Efficiency

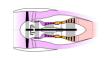


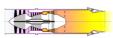
Drawing enthalpy-entropy diagrams to scale can be very helpful for understanding the effects of changes. It is much better than using complex equations!

















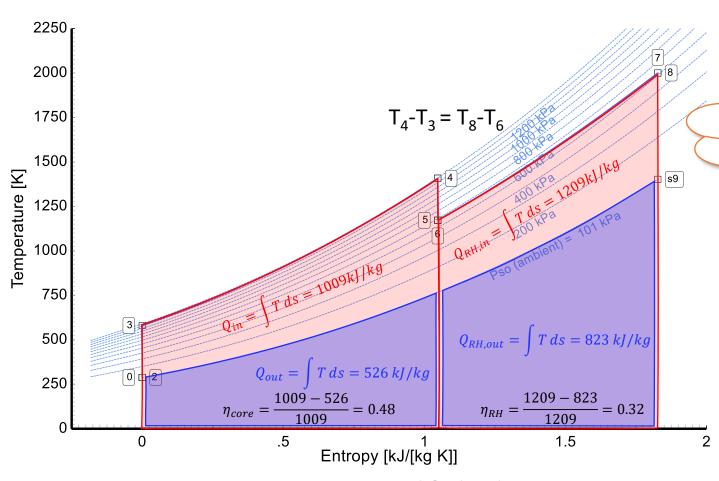




Temperature-Entropy Diagram

Visualize the Amount of Heat Transferred

Why is afterburner SFC much larger than dry SFC?



Drawing temperature-entropy diagrams to scale can help to improve understanding of thermodynamics. Presenting results in graphical form is much more effective than using complex equations!











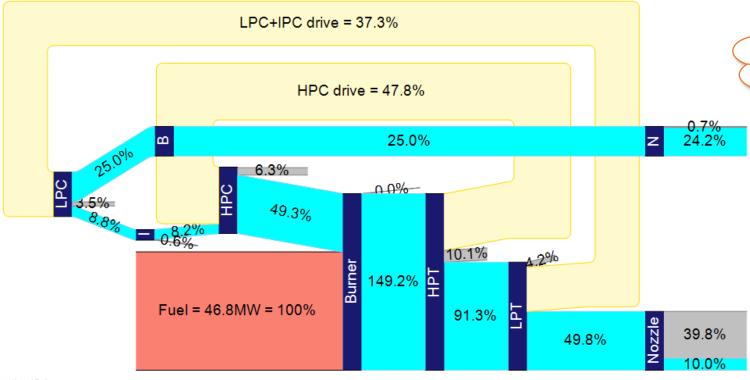








Energy Flow - Sankey Diagram CFM56-3 Take Off



The Sankey diagram clearly shows that the small gas generator dominates the energy flows in a turbofan.

SL static, ISA

September 2025

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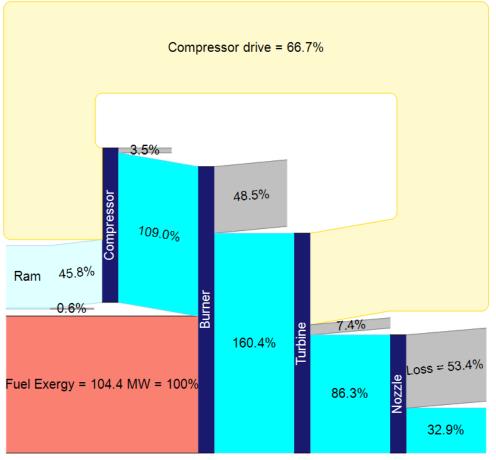






Work Potential - Exergy Diagram

Turbojet, Mach 2, 11km



A turbojet could be an attractive option for the propulsion system of a supersonic fighter aircraft.

An exergy diagram shows where losses in terms of work potential occur, which is important to consider when analysing the system.













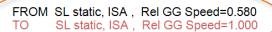


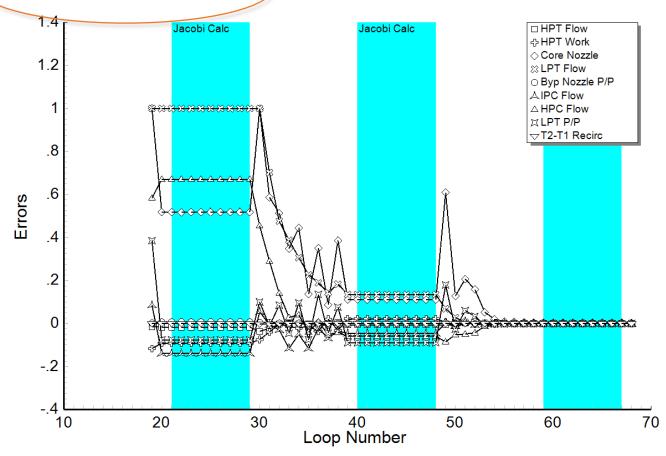






The Iteration Progress





Off-design calculations require multidimensional, iterative algorithms. Sometimes, convergence problems are encountered. Solving these problems is very important in practice. Graphics can be helpful.























Is It Magic?

De-Mystify your Performance Program!

That's what a lecturer's really for – not teaching complex equations that don't actually apply to the day-to-day work of a performance engineer.



T-



















A good bedtime read ...

